

- 86 J-137-J-138-92.2-KC=63φ
 145 J-B7-J-128-142.8-KC=75φ
 J-137-J-128 11.7-I.L. (Crossing)=63φ
 J-128-J-135-121.9-I.L.=63φ -
 206 J-128-J-135-37.0-M=KC=63φ
 J-135A-J-135B-54-M=KC=63φ
 J-135A-J-135B-60-M=J.L. (Crossing)=63φ
 41 J-136-J-135-134-M=KC=63φ
 40 J-135-J-130-40.1-M=KC=63φ
 66 J-130-J-132-84.5-M=KC=63φ
 J-130A-J-130B-61.4-M=KC=63φ
 247 J-130-J-126-50.2-Bot=63φ
 J-130-J-126-28.1-KC=63φ
 J-130-J-126-148.1-KC=63φ
 133 J-128-J-126-20.0-I.L.=75φ
 J-128-J-126-19.7-Culvert=75φ
 J-128-J-126-98.4-M=KC=75φ
 198 J-126-J-56-20.1-KC=75φ
 J-126-J-56-18.5-Bot (Crossing)=75φ
 J-126-J-56-7.0-Bot (Crossing)=75φ
 299 J-56-J-38-298.2-M=KC=160φ
 223 J-56-J-122-91.1-KC=160φ
 J-56-J-122-56.9-I.L.=160φ
 J-56-J-122-76.4-KC=160φ
 J-56-J-122-4.2-Bot=160φ
 129 J-122-124-6.0-M=Bot (Crossing)=160φ

- J-122-J-124-176.0-M₂KC=160φ
 13 J-124-J-125-92.6-KC=63φ
 J-124-J-124A-14.9-KC=~~63φ~~ 160φ
 J-124A-J-124B-39.1-KC=63φ
 162 J-124A-J-124B-174.3-KC=160φ
 9 J-143-J-142-200.5-M₂ 63φ
 182 J-143-J-145-113.2-KC=160φ
 J-143-J-145-5.9-B₀T₀CROSSING=160φ
 9 J-146-J-145-7.6-M₂ KC=160φ
 235 J-145-J-144-230.6-M₂KC=75φ
 J-145-144-9.8-M₂B₀T₀CROSSING=75φ
 345 J-144-J-149-298.6-M₂KC=140φ
 J-144-J-149-63.2-M₂2L₀-140φ
 351 J-149-J-154-6.0-M₂B₀T₀CROSSING=140φ
 J-149-J-154-152.1-KC-(B₀F)=140φ
 J-149-J-154-214.7-B₀F=140φ
 J-154-J-164-91.6-KC-(B₀F)=110φ
 332 J-154-J-164-140-KC=110φ
 J-164-J-166-680.6-KC=160φ
 92 J-164-J-166-31.6-M₂B₀F=160φ
 J-166-J-166A-20.2-M₂KC=75φ
 J-166A-J-170-276.0-M₂KC=75φ
 88 J-170-J-172-92.3-M₂KC=75φ
 129 J-172-J-166-128.7-B₀F=160φ
 J-166A-J-167-29.1-KC=75φ
 84 J-164-J-160-100.9-KC=160φ

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- 198 J-154-J-160-110.1-KC=63 ϕ
 J-154-J-160-92.2-Bot=63 ϕ
 50 J-154-J-153-51-KC=~~160~~ 140 ϕ
 301 J-153-J-158-292.9-KC=160 ϕ
 216 J-153-J-146-214.9-M=160 ϕ
 325 J-144-J-122-47.1-M=KC=140 ϕ
 J-144-J-122-6.8=Culvert ex-
 J-144-J-122-192.2-140 ϕ
 J-144-J-122-8.1-M=2 Culvert ex-140 ϕ
 J-144-J-122-80.6-M=KC=140 ϕ
 55 J-224-J-228-53.2-M=Bot=90 ϕ
 10 J-228-J-231-10.8-M=Bot=90 ϕ
 J-228-J-225-3.1-M=Bot=63 ϕ
 98 J-228-J-225-89.4-M=KC=63 ϕ
 162 J-231-J-232-59.5-M=KC=63 ϕ
 155 J-231-J-233-162.5-M=KC=63 ϕ
 J-224-J-228-5.6-M=Bot (Crossing)=90 ϕ
 47 J-224-J-227-51.7-M=KC=90 ϕ
 J-227-J-227-24.3-M=KC=63 ϕ
 -27-J-227-J-230-103.4-M=Bot=90 ϕ
 J-230-J-231-45.2-M=KC=90 ϕ
 101 J-230-J-226-62.1-M=KC=90 ϕ
 124 J-226-J-229-175.9-M=KC=63 ϕ
 259 J-230-J-236-177.4-M=Bot=90 ϕ
 216 J-236-J-239-204.7-M=KC=63 ϕ
 398 J-236-J-223A-225.4-M=KC=90 ϕ
 J-223A-223B-68.7-M=KC=90 ϕ

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- J-23A J-23- 172.4 - KC 290¢
234 J-223 J-234A- 182.9 - KC 290¢
J-234A-234B- 205.8 - KC 275¢
J-234B- J-234C- 27.3 - KC 275¢
J-234B- J-234D- 70.1 - KC 275¢
231 J-237- J-239- 45.5 - M₂ KC 63¢
J-234- J-234A- 55.3 - M₂ KC 275¢
444 J-223- J-193- 447.9 - M₂ KC 290¢
J-223- J-193- 7. M₂ B.T.C. Cross SWG 290¢
93 J-193- J-195- 7.4 - Calure Alex 2140¢
31 J-193- J-195- 88.9 - KC 140¢
J-195- J-196- 29.1 - M₂ KC 140¢
17 J-196- J-197- 54.9 - M₂ KC 63¢
98 J-192- J-195- 98.4 - M₂ KC 140¢
61 J-192- J-193- 65.6 - M₂ KC 290¢
J-192- J-192A- 45.8 - M₂ KC 140¢
J-192A- J-192B- 24.3 - M₂ KC 63¢
J-192A- J-181- 172.5 - M₂ KC 140¢
113 J-181- J-187- 44.7 - M₂ J.O.L. - 140¢
134 J-187- J-193- 135.1 - M₂ KC 140¢
J-187- J-193- 5. M-B.T.C. Cross SWG 140¢
SS J-181- J-179- 29.7 - J.O.L. - 160¢
J-181- J-179- 55.3 - C.Road - 160¢
142 J-179- J-180- 160.3 - M₂ KC 75¢
148 J-179- J-178- 151.5 - M₂ C.Road - 160¢
361 J-178- J-206- 373.2 - M₂ C.Road - 160¢

- 130-J-206-J-213-184.52-B.T. Road-2160p
 57 J-213-J-214-52.2-M2 KC280p
 82 J-214-J-216 114.5-M2 KC=63p
 36 J-214-J-215-61.2-M2 KC=63p
 90.2-M2
 J-213-J-218-31.1-M-B.T. Road-14p
 179 J-213-J-218-103.3-M2 KC2140p
 156 J-224-J-218-206-1-M2 KC2110p
 414 J-172-J-178-423.2-M2 (C Road)-160p
 362 J-217-J-223-366.3-M2 KC290p
 216-J-196-J-198-252.2-M2 KC2140p
 138-J-198-J-199-141.5-BoE2140p
 148-J-199-J-207-29.2-BoE=75p
 J-199-J-207-5.5-Lo-75p
 J-199-J-207-95.0-KC-75p
 J-199-J-207-41.0-BoE=75p
 J-199-J-207-29.0-KC=75p
 184-J-210-J-204-56.0-M2 KC275p
 83 J-11-J-11-61.7-M2 KC263p
 12 J-11-J-12-95.3-M2 KC263p
 54 J-11-J-14-93.2-M2 KC263p
 103 J-5-J-6-183.4-M2 KC263p
 200 J-9-J-17-228.3-M2 KC2200p
 108 J-17-J-23-101.2-M2 KC263p
 40 J-23-J-22-40.2-M2 KC2200p
 36 J-22-J-20-35.4-M2 KC2200p
 51 J-20-J-21 50.5-M2 KC263p
 56 J-20-J-17-42.4-M2 KC2200p

- 167- J-22-J-38- 177.2- M₂ KC= 1600
 J-22-J-38- 5. M₂ B.T. CROSSING= 630
 137 J-1-J-3- 67.2- KC= 630
 J-1-J-3- 86.2- BofE= 630
 152 J-23-J-27- 158.8- M₂ 2000 = B.T. Road
 J-27-J-30- 5- M₂ B.T. Road= 630
 322 J-27-J-30- 273.3- M₂ KC= 630
 168 J-27-J-37- 172.3- M₂ B.T. Road= 2000
 146- J-37-J-39- 34.1- M₂ KC= 630
 J-37-J-37A- 115.6- M₂ KC= 630
 J-37A-J-37B- 106.8- M₂ KC= 630
 472- J-37-J-42- 481.1- M₂ B.T. Road= 2000
 14 J-42-J-43- 98. M₂ (I.L.) = 2000 KC
 J-42-J-43- 88.1- M₂ KC= 2000
 J-43-J-43A- 136.9- M₂ KC= 630
 J-43-J-41- 303.2- M₂ KC= 2000
 138 J-41-J-36- 137- M₂ KC= 750
 42 J-36-J-34- 67.2- M₂ KC= 630
 175- J-36-J-28- 207.8- M₂ KC= 630
 453- J-41-J-122- 472- M₂ BofE= 1400
 303 J-42-J-48- 211.8- M₂ B.T. Road= 1400
 160 J-48-J-49 156.5- M₂ KC= 630
 136- J-48-J-57- 110.5- M₂ B.T. Road= 1400
 J-48-J-57- 25.6- M₂ I.L. = 1400
 115 J-57-J-58- 55.8- M₂ BofE= 630
 194 J-63-J-68- 114.9- M₂ KC= 750

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- 40 J-68-J-69-321-M-KC=75d
 121 J-~~82~~ J-69-185-M-KC=63d
 69 J-82-J-71-62-M-BoE=275d
 46 J-69-J-~~67~~ 81.2-M-KC=75d
 142 J-57-J-62-139.1-M-ZIL-140d
 242 J-62-J-90-310-M-KC=63d
 213 J-62-J-92-220-M-BoT.Road-140d
 93 J-92-J-95-93.6-M-KC=75d
 116 J-95-J-98-135.9-M-KC=63d
 48 J-95-J-96-5-M-BoT.Crossing-63d
 J-95-J-96-39-M-KC=63d
 197 J-92-J-94-201.7-M-KC=110d
 138 J-92-J-101-142.2-M-BoE=110d
 68 J-101-J-104-70.2-M-KC=110d
 116 J-104-J-106-119.6-M-BoE=110d
 12 J-106-J-107-15.6-M-KC=110d
 75 J-107-J-109-20.7-M-KC=63d
 89 J-107-J-112-88.9-M-KC=63d
 J-116-J-119-3-M-BoE(Rossing)-63d
 35 J-116-J-119-69-M-KC=63d
 95 J-116-J-113-89-M-KC=63d
 39 J-116-J-108-41.6-M-KC=63d
 45 J-108-J-109-48-M-BoE=75d
 41 J-109-J-115-20.8-M-KC=63d
 75 J-109-J-106-39.6-M-KC=75d
 112 J-108-J-103-11-M-KC=75d
 J-108-J-103-6-M-Culture to go-75d

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This Pipeline is yet to be Laid in the Ground —

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197 J-105-J-124-203.2-M₂ KC=75φ
92 J-163-J-161-89.6-M₂ KC=75φ
76 J-161-J-162-112.3-M₂ KC=63φ
83 J-173-J-174-107.5-M₂(I.L.)-KC=63φ
40 J-59-J-61-75.1-M₂(I.L.)-KC=63φ
44 J-85-J-86-41.1-M₂ KC=63φ

It hasn't happened
yet but it will happen